

DAMAGE SELF-SENSING BEHAVIOR OF BASALT FIBER REINFORCED



POLYMER COMPOSITES MODIFIED BY ELECTROPHORETIC DEPOSITION

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Abstract

In this work, basalt fiber reinforced polymer (BFRP) with enhanced electrical, mechanical properties and in-situ damage self-sensing capability was prepared using carboxylic carbon nanotubes (COOH-CNTs) modified BF fabrics via electrophoretic deposition (EPD) at different voltages. The BFRP with BF fabrics modified at a deposition voltage of 20 V (EPD20-BFRP) showed the lowest electrical resistivity. Compared with unmodified BFRP, the tensile and flexual moduli of EPD20-BFRP increased by 37.5% and 14.9%, respectively. Single-layer EPD20-BFRP exhibited a high gauge factor (GF) of 44.3 during tensile damage self-sensing. The acoustic emission (AE) signals during tensile and flexual damage process agreed well with the relative resistance changes (RRC), which confirmed different damage stages within loading process, such as elastic deformation, damage evolution, crack coalescence, and complete fracture. The multi-layer BFRP containing a single-layer EPD20-BFRP on the upper or lower surface of laminate exhibited distinct electrical signal responses subjected to the flexural loading.

Methods



Fig. 1 The modification process: (a) The original BF fabric, (b) BF fabric -washed, (c and c1-4) the EPD process, (d) the EPD-BF fabric, (e) structure of single-layer EPD-BFRP, (f) structure of multi-layer BFRP, (g) schematic diagram of tensile specimen, (h) schematic diagram of flexure specimen.

Loading AE probe direction

Morphology



Fig. 2. SEM images showing: (a–f) The surface morphologies of the BFs subject to deposition voltages of 0, 5, 10, 15, 20, and 25 V, respectively; (g and h) BFRP and EPD20-BFRP failure surfaces, respectively; and (i and j) failure sections of BFRP and EPD20-BFRP

Mechanical properties



Electrical properties

 Table. 1 The resistivity of EPD-BFRP in different directions

Sample	Resistivity (kΩ·mm ⁻¹)				
	In-plane	Through-layer			
BFRP	N/A	N/A			
EPD5-BFRP	44.2(±2.4)	895.3(±9.4)			
EPD10-BFRP	39.1(±3.1)	600.4(±7.0)			
EPD15-BFRP	36.8(±2.1)	313.78(±3.8)			
EPD20-BFRP	34.8(±1.6)	233.4(±7.1)			
EPD25-BFRP	35.1(±3.3)	247.6(±1.3)			

Table. 2 Change ratio of the EPD-BFRPs mechanical properties at different EPD deposition voltages								
Sample	ΔEt (%)	Δσt (%)	$\Delta \epsilon_t$ (%)	$\Delta E_{\rm f}$ (%)	$\Delta \sigma_{\rm f}$ (%)	Δ£f (%)		
EPD 5-BFRP	+ 9.9	+ 6.6	+ 2.0	+ 3.5	+ 6.9	+ 4.5		



Damage self-sensing properties

Fig. 3 Mechanical properties of the BFRPs produced at different EPD deposition voltages: (a) tensile property and (b) flexural property.





Fig.4 Schematic diagrams of the damage and electrical property evolution of EPD-BFRP. (a) tensile load applied, (b) flexural load applied, (c1-c6) tensile failure process and (d1-d6) flexural failure process.



40

10.0

S-S curve

AE signal

Strain (%)

• RRC

Conclusions

A BFRP with damage self-sensing property was prepared by electrical deposition of CNT. Single-layer EPD20-BFRP exhibited a high gauge factor (GF) of 44.3 during tension and 14.6 during flexure. For the functional layer at lower surface, the RRC increased lineary in elastic deformation and damage evolution stages. The multi-layer BFRP containing single-layer EPD20-BFRP exhibited distinct RRC responses subjected to the flexural loading on the upper or lower surface. This behavior can be used to identify the direction of stress applied to the structure. The results obtained in this work indicate that EPD-BFRP is suitable for in-situ damage detection of **BF** reinforced composite materials.

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