

BICOMPONENT PP FIBERS FOR SUSTAINABLE MINERAL BONDED STRAIN HARDENING COMPOSITES

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Motivation

- existing reinforced concrete structures reveal low resistance to impact loading, such as shock, collision, or explosion

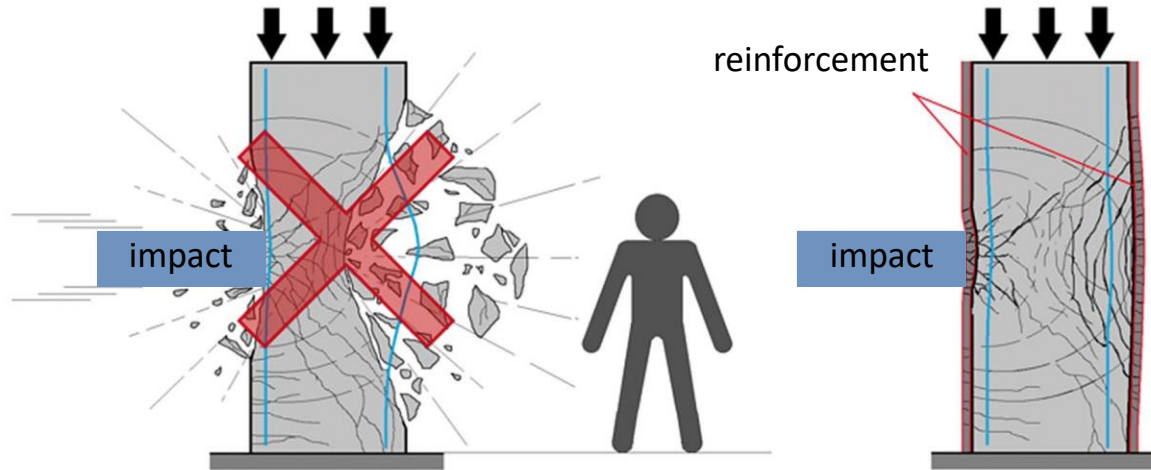


impact
loading



Research Target

- application of thin layers of strengthening material using innovative, mineral-bonded composites
- economically and ecologically approach



Research Training Group

Mineral-bonded
composites for enhanced
structural impact safety

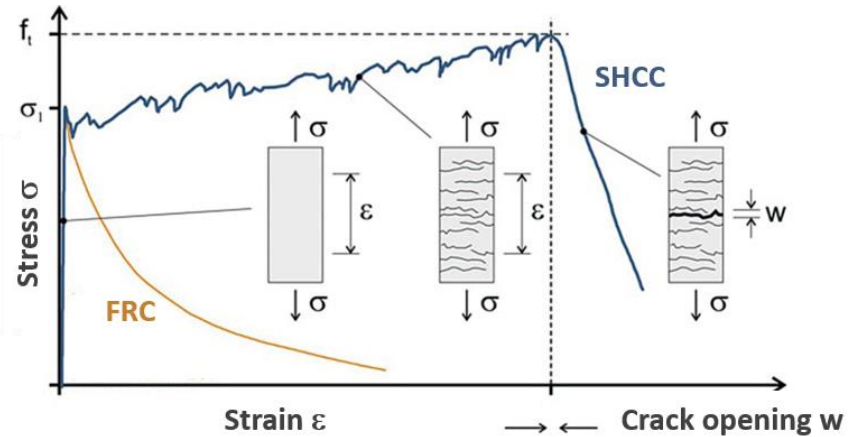
<https://www.grk2250.de/>

State of the art

- strain-hardening concrete composites = polymer fibers (2 vol.-%) + concrete matrix
- fiber diameter 10-20 μm , widely used PVA, HDPE, PP



micro-crack bridging for high energy absorption

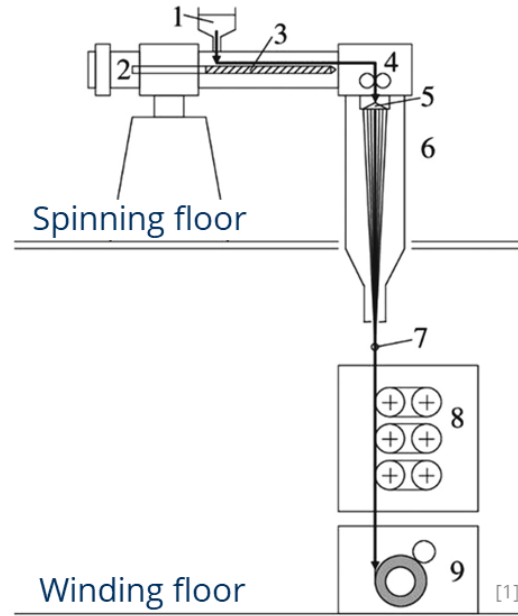


Approach

Polypropylene fibers (PP):

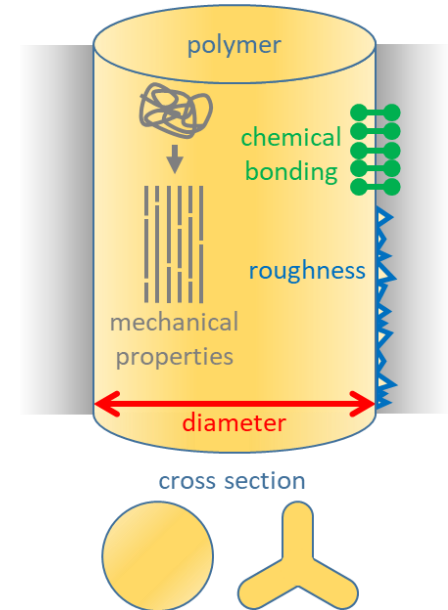
- high availability, cost-effective
- alkali-resistant
- production process can use recycled PP

Melt spinning



[1] Brüning, H. Adv Polym Sci (2018) 282: 1–34

Fundamental research on tailored fibers

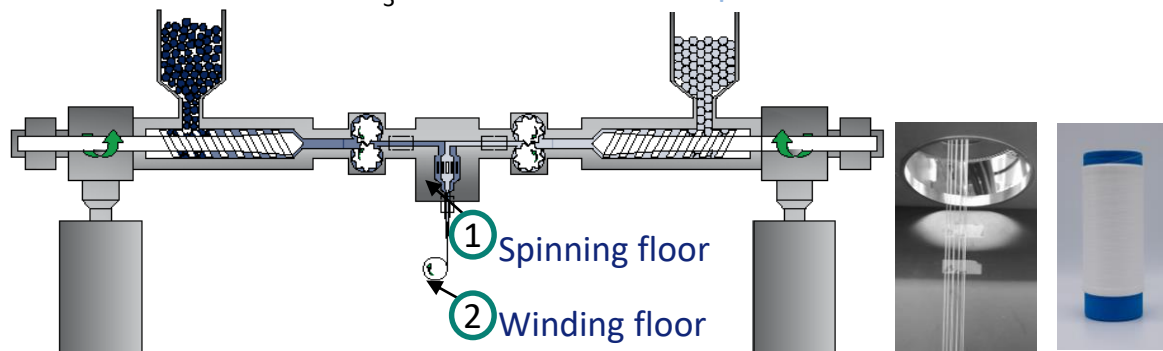


Approach

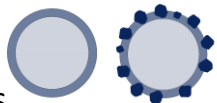
- Aim: Improvement of mechanical interlocking combined with high tensile strength
- → Development of bicomponent PP-fibers with increased surface roughness

Shell material: PP + CaCO₃

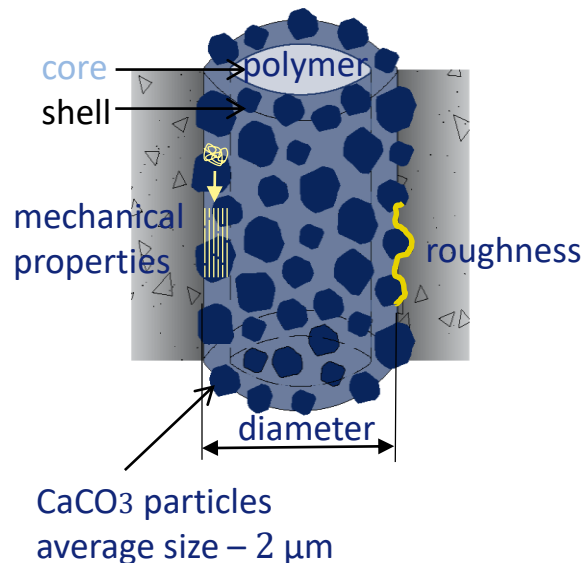
Core material: pure PP



- Spinneret
Eleven holes
- Online drawing
Enhanced mechanical properties



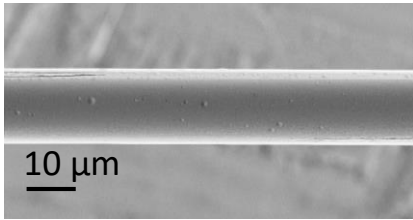
- Chamber size
Endless fibers
- Spin finish
Favisan UF 1625: 90% water
+ 10% Tenside composition



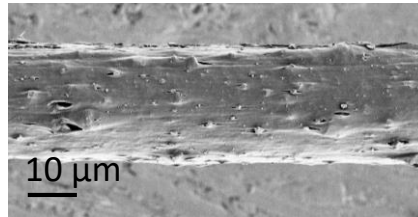
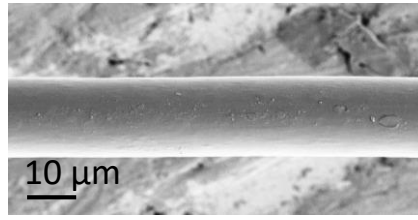
Experimental plan

- core/shell ratio 75/25
- incorporating CaCO_3 -particle content
- dies size 0.3 x 0.6 mm
- $v = 2400$ m/min
- drawing ratio $\text{DR}=3$

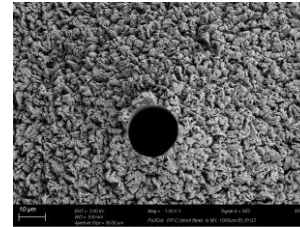
Commercial PP-fiber
(mono), $d = 19.8 \mu\text{m}$



PP + PP,
 $d=27.61 \mu\text{m}$



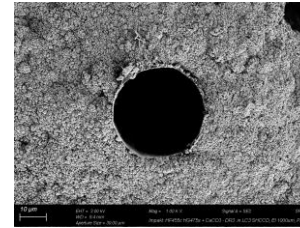
PP + 10 vol.% CaCO_3 ,
 $d=28.37 \mu\text{m}$



M1 matrix

GRK2250/I

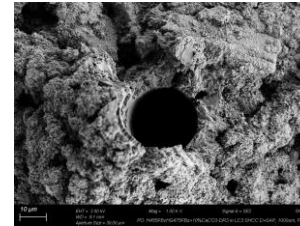
- basis model mix
- high strength matrix
(Dr. Curosu I. 2016)



FRLC₃ matrix

Optimized model mix

- ↑ sustainability
- LC₃: lower CO_2 emissions,
- ↑ micro-mechanical properties



FRLC₃ + SAP matrix

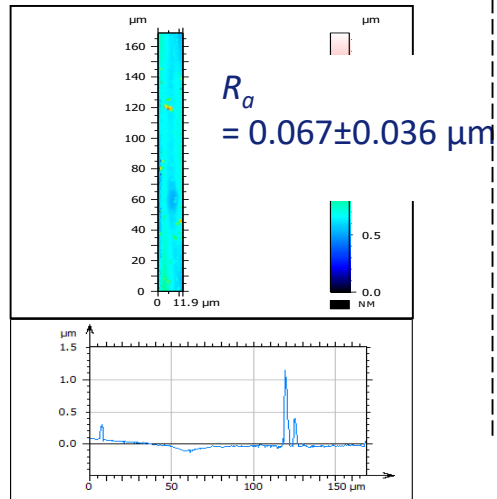
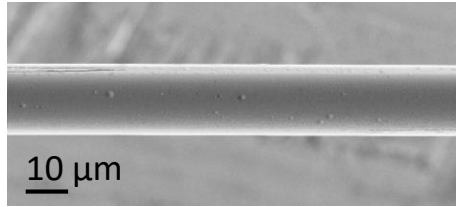
Superabsorbant polymer

- ↑ porosity →
- ↑ strain-hardening effect

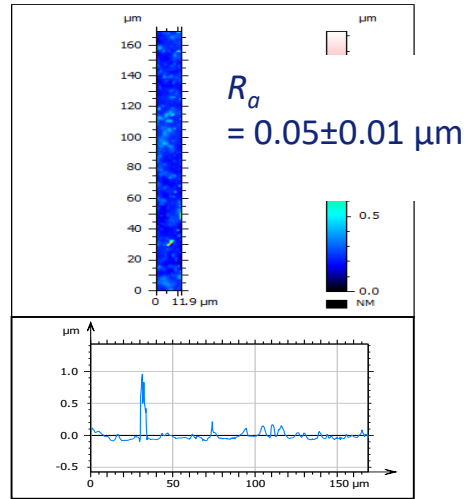
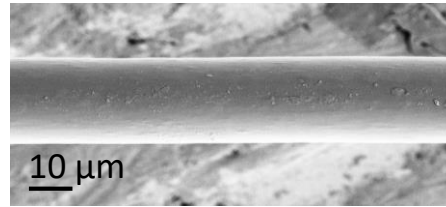
Results – Fiber spinning trials

Analysis of surface morphology and roughness

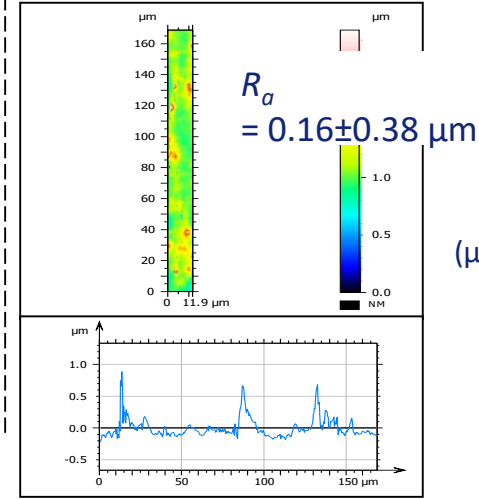
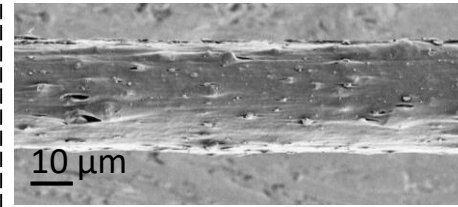
Commercial PP-fiber (mono),



PP + PP_DR3



PP + 10 vol.% CaCO₃_DR3



Confocal Microscope
(μSurf expert, Nanofocus AG)

R_a = arithmetic mean
deviation of the surface

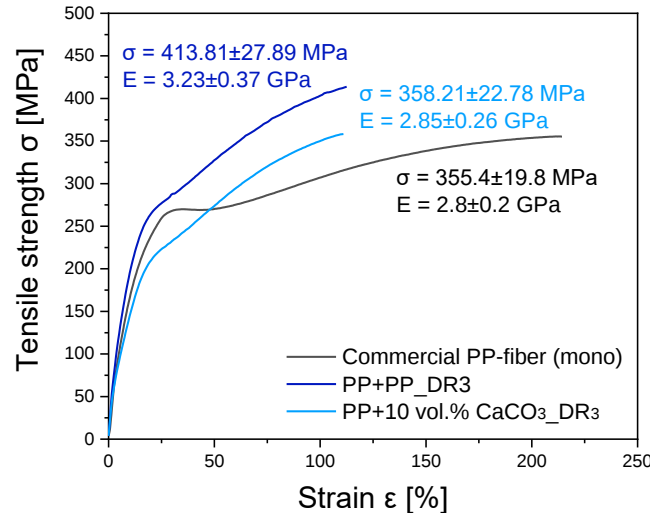
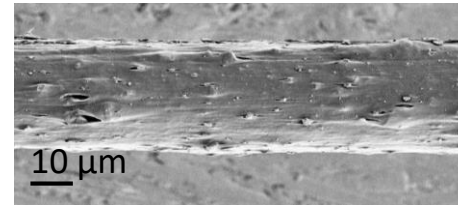
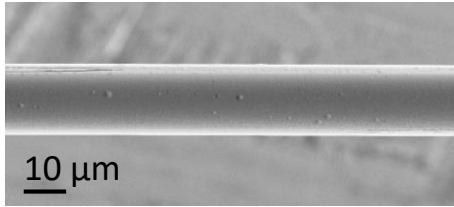
Results – Fiber spinning trials

Analysis of mechanical properties

Commercial PP-fiber (mono),

PP + PP_DR3

PP + 10 vol.% CaCO₃_DR3

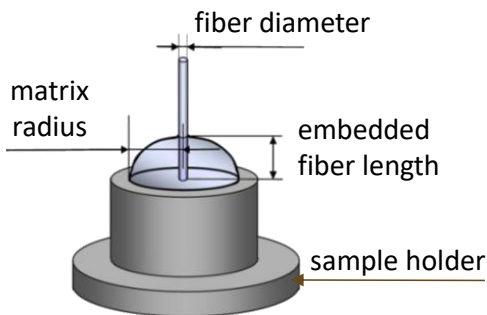


FAVIMAT+ (Textechno)

- Clamping length (10 mm)
- Velocity (5 mm/min)

Single fiber pull-out test (SFPO)

Sample preparation



computer assisted embedding, $l_e = 1000 \mu\text{m}$

FRLC3 (normal strength r
Beigh B.A.M. et al.

CEM I 52,5 R-SR3/NA (2) (Holc

Limestone (Saxodol 90 LE)

Clay (Liapor)

Gypsum (D) (Fluka (Honeywell))

Quartz sand 0.06–0.2 mm (BCS 41.

H2O

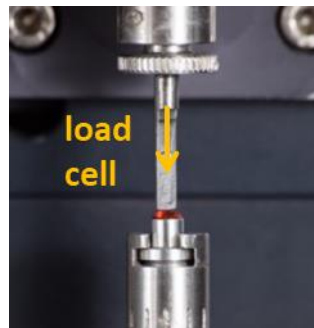
FM MG ACE 460 (BASF)

VMA (SIKA)

FRLC3 +
SAP

Testing

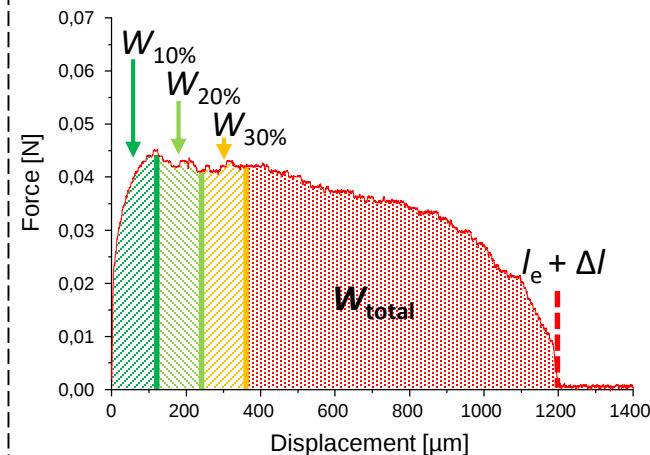
quasi-static, $v=1,000 \mu\text{m/s}$



dynamic, $v=10,000 \mu\text{m/s}$



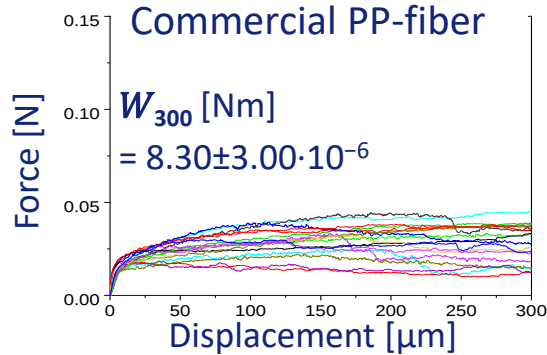
Evaluation



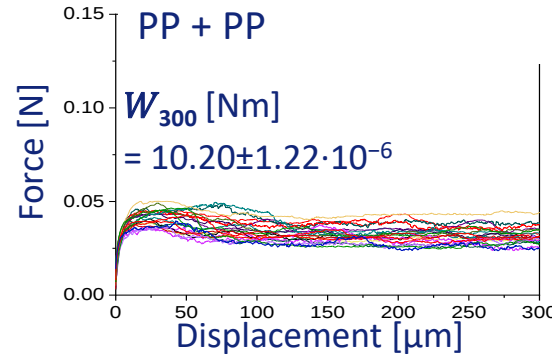
$$W_{\text{total}} = W_{\text{chemical bond}} + W_{\text{friction}} + W_{\text{fiber elongation}} + W_{\text{fiber surface deformation}}$$

Results – Quasi-static single fiber pull-out test (Q-SFPO)

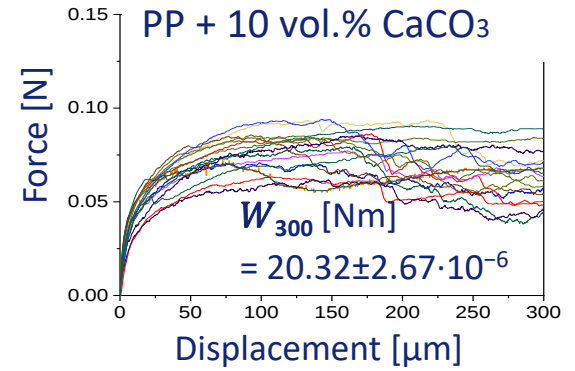
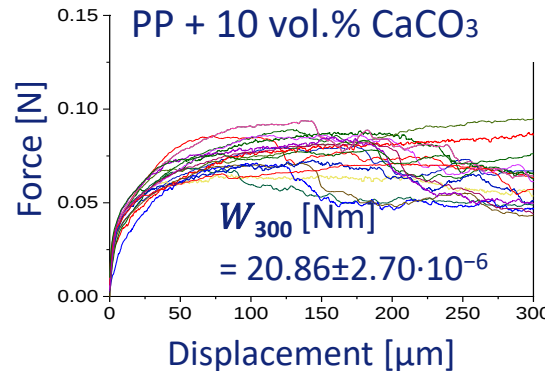
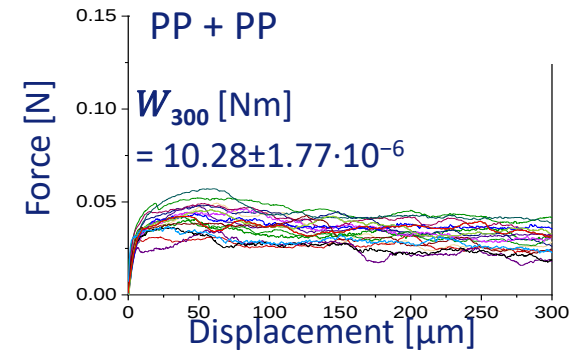
– in M1 matrix



– in FRLC3 matrix

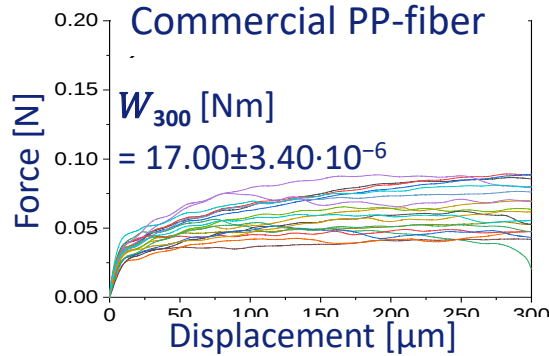


– in FRLC3+SAP matrix

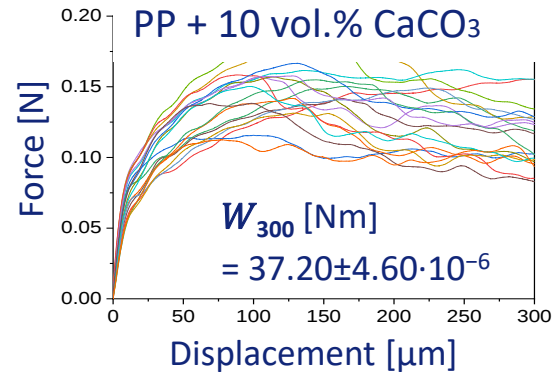
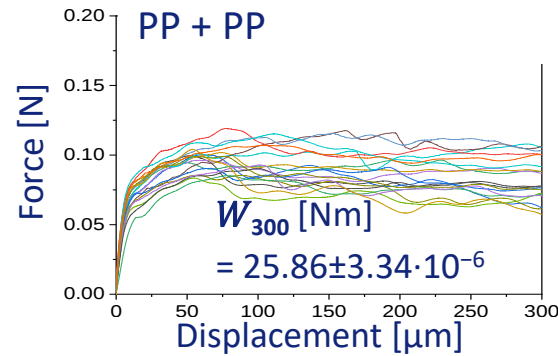


Results – Dynamic single fiber pull-out test (D-SFPO)

– in M1 matrix

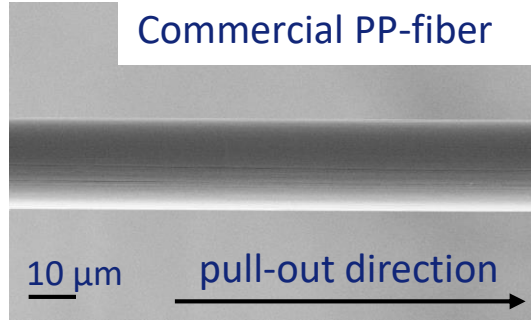


– in FRLC3 matrix

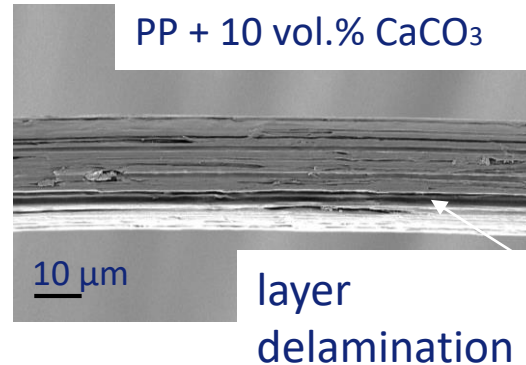
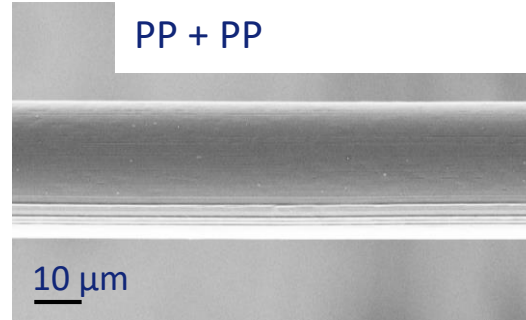


Results – Surface morphology after Q-SFPO

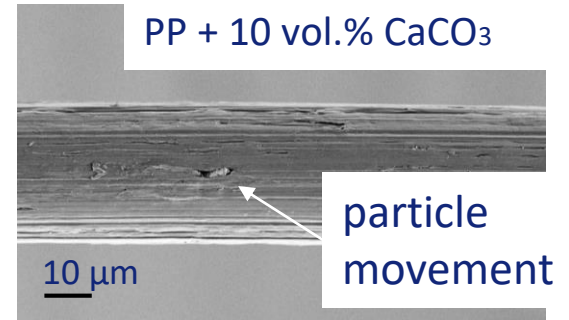
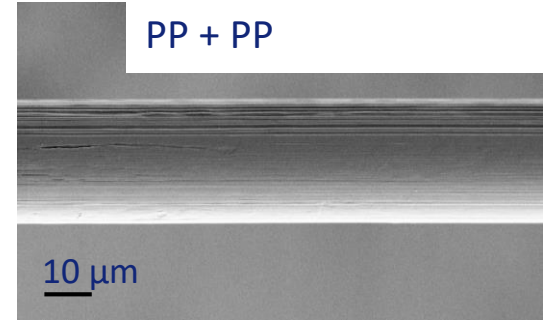
– in M1 matrix



– in FRLC3 matrix

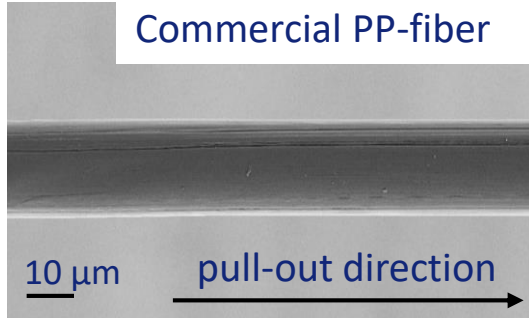


– in FRLC3+SAP matrix

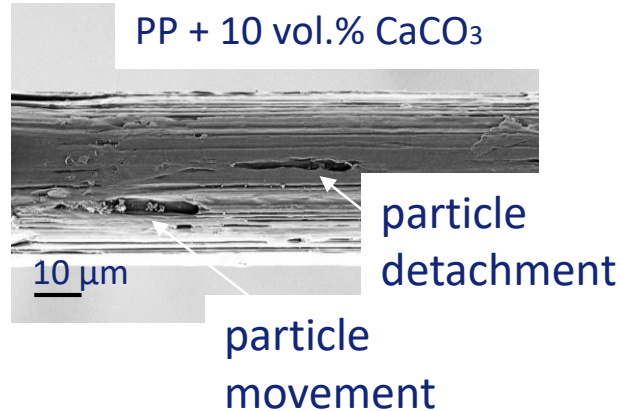
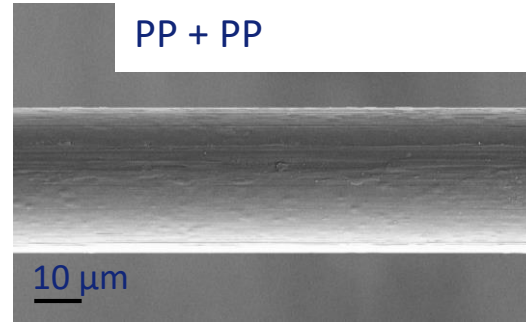


Results – Surface morphology after D-SFPO

– in M1 matrix

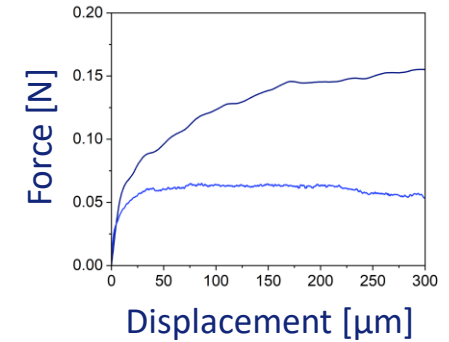


– in FRLC3 matrix



Summary and Outlook

- enhanced energy absorption in FRLC₃ matrix and after SAP addition using rough PP bicomponent fibers compared to 'smooth' monocomponent PP fiber in M1 matrix
- no fiber bridging improvement after SAP addition compared to FRLC₃ regime
- 'smooth' bicomponent PP fibers showed slight bridging improvement in FRLC₃ matrix, even with SAP addition
- composites containing rough PP bicomponent fibers exhibit a propensity for strain-hardening behavior
- SAP utilization enhances the potential for stress transfer through multiple cracking
- rough fibers improve composite properties with less volume fraction



Micro-scale analysis



Macro-scale analysis



BC2.5%



S-BC2.5%

Thank you for your kind attention!

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