

# NUMERICAL INVESTIGATION OF THE VIBRATION BEHAVIOR OF A COMPOSITE DRILL TUBE

ICCM23 International Conference on Composite Materials Belfast 2023

---

M. Kurkowski<sup>1</sup>, S. Michel<sup>2</sup>, J. Summa<sup>3</sup>, H.-G. Herrmann<sup>3,4</sup>,  
D. Biermann<sup>2</sup>, A. Spickenheuer<sup>1</sup>, M. Stommel<sup>1,5</sup>

<sup>1</sup> Leibniz-Institut für Polymerforschung Dresden e. V., Dresden, Germany,

<sup>2</sup> Institute of Machining Technology, TU Dortmund University, Dortmund, Germany,

<sup>3</sup> Fraunhofer Institute of non-destructive testing IZFP, Saarbrücken, Germany,

<sup>4</sup> Chair for Lightweight Design, Saarland University, Saarbrücken, Germany,

<sup>5</sup> Faculty of Mechanical Engineering, Institute of Material Science, Chair of Polymer Materials,  
Technische Universität Dresden, Dresden, Germany

# BTA Deep Hole Drilling



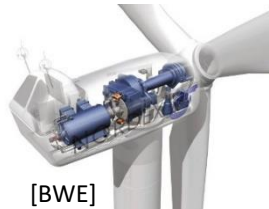
## Typical applications

### Plastic processing



Double twin-screw  
extruder barrel

### Renewable energy



Rotor and generator shafts



### Lightweight design



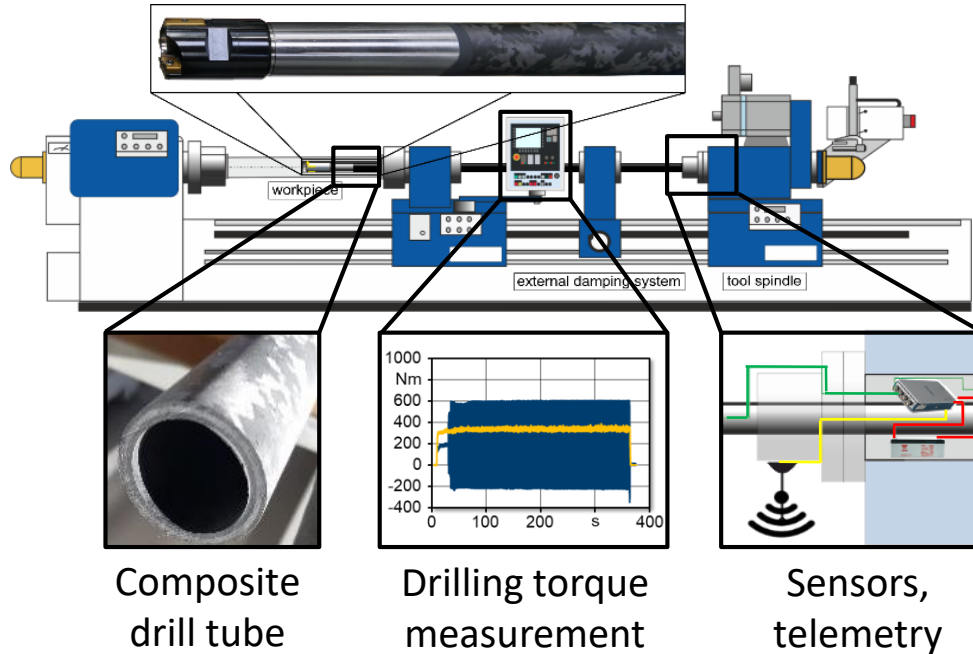
Aircraft landing legs

### Chemical industry



High-pressure pipes

# Composite Drill Tubes for BTA Deep Hole Drilling



## Aim of the project:

- Vibration-damping
- Weight reduction
- Structure-integrated sensors
- Hybrid connection concept

# Design and Manufacture of the Composite Drill Tube

Geometry:

$d_i = 40 \text{ mm}$ ,  $d_a = 51 \text{ mm}$ ,  $l = 2650 \text{ mm}$

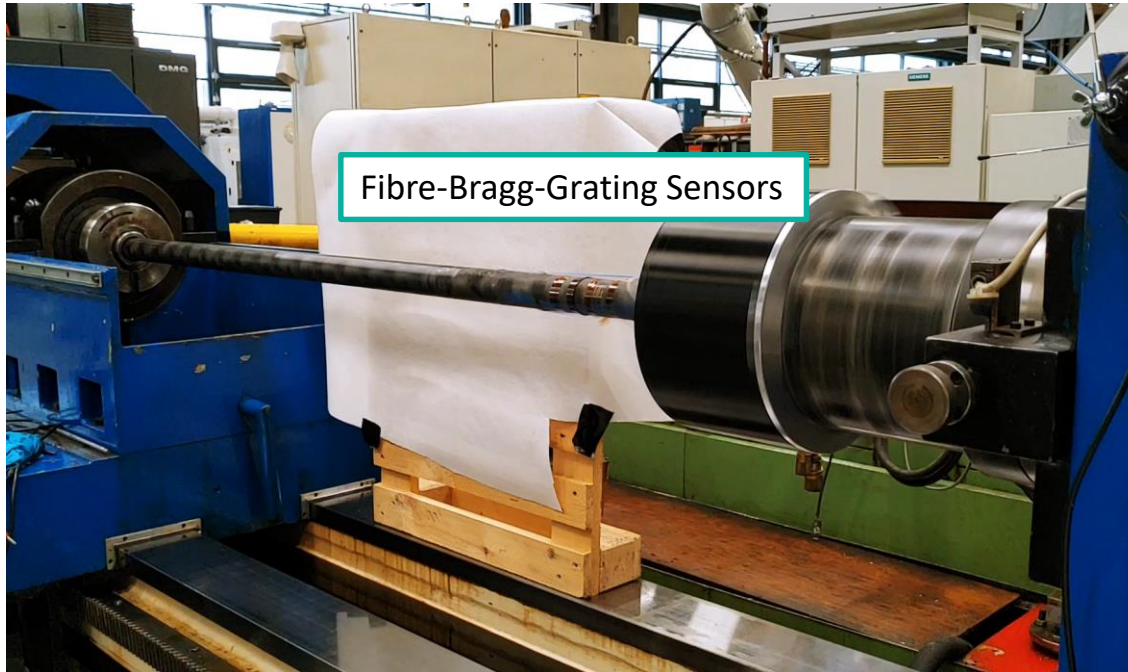
Laminate structure:

$[\pm 6_2^{CF1} / \pm 45_2^{GF} / \pm 45_2^{CF1}]$

| Name   | Material                                                     | Stiffness<br>[GPa] |
|--------|--------------------------------------------------------------|--------------------|
| CF1    | STS40 F13, 24K, 1600 tex<br>(Toho Tenax)                     | 240                |
| CF2    | Dialead K63712, 12K, 2000 tex<br>(Mitsubishi Chemical)       | 640                |
| GF     | SE1200, 2400 tex (Owens Corning)                             | 82                 |
| Matrix | Epikote MGS RIMR 935 with Epikure -<br>MGS RIMH 937 (Hexion) | -                  |



# Process Parallel Vibration Measurement



Video of the rotating drill tube with sensors in drilling test



Mounting the platform and the drill tube on the drill chuck

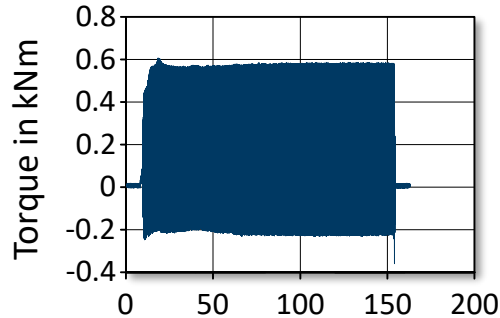


Platform with interrogator (red) and two measuring amplifiers (white)

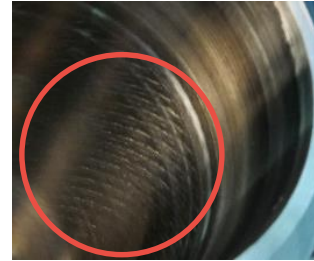
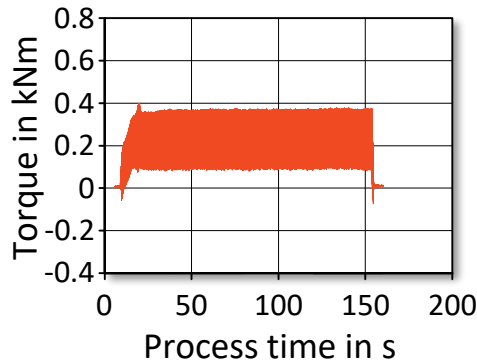


# Results of the Drilling Tests

Steel  
drill tube



Composite  
drill tube



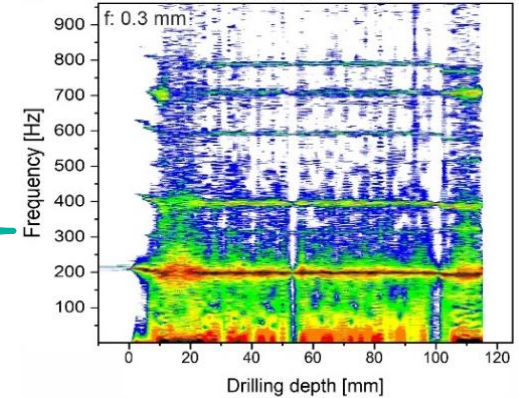
Chatter marks caused  
by torsional vibrations



Example images

Improved surface quality

FFT analysis over drilling depth



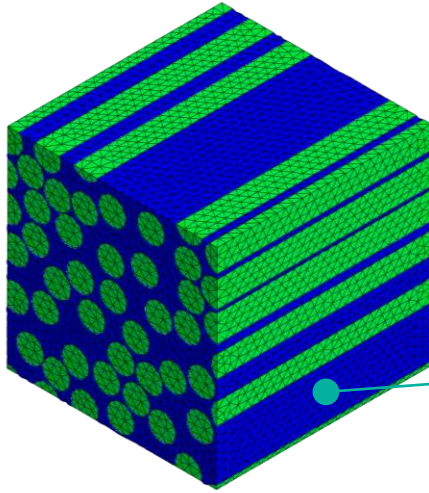
Amplitude of FFT (Drilling Torque) [Nm]

Process parallel  
vibration analysis

Vibration damping due to composite use

**How can the material damping of the composite drill tube be simulated?**

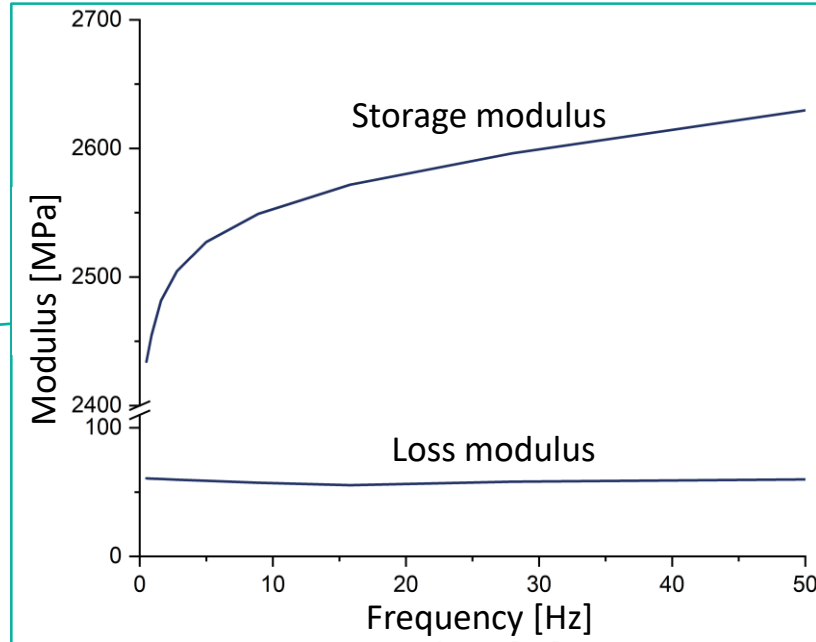
# Model Approach



## Directional material damping

- Fibers: no damping (model)
- Epoxy resin: damping (visco-elastic)

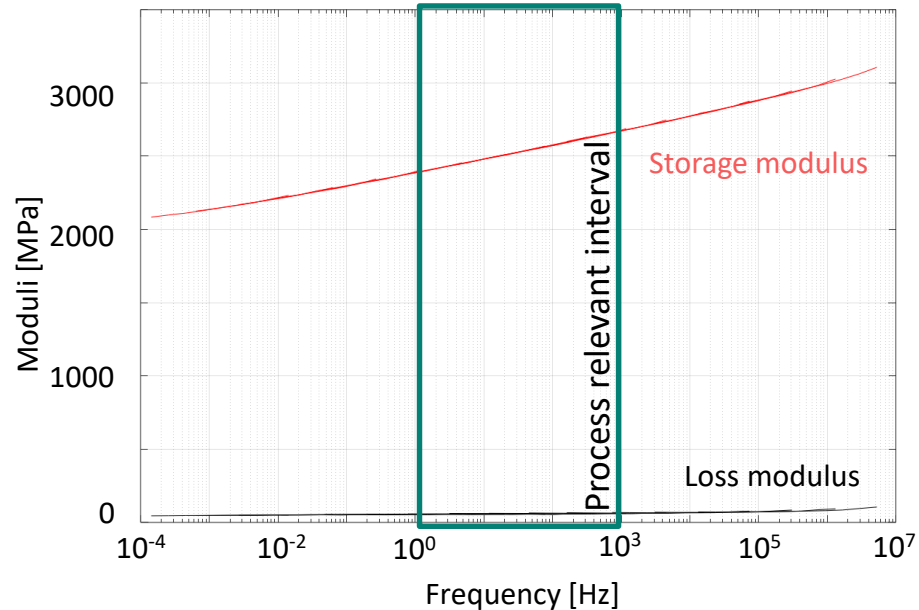
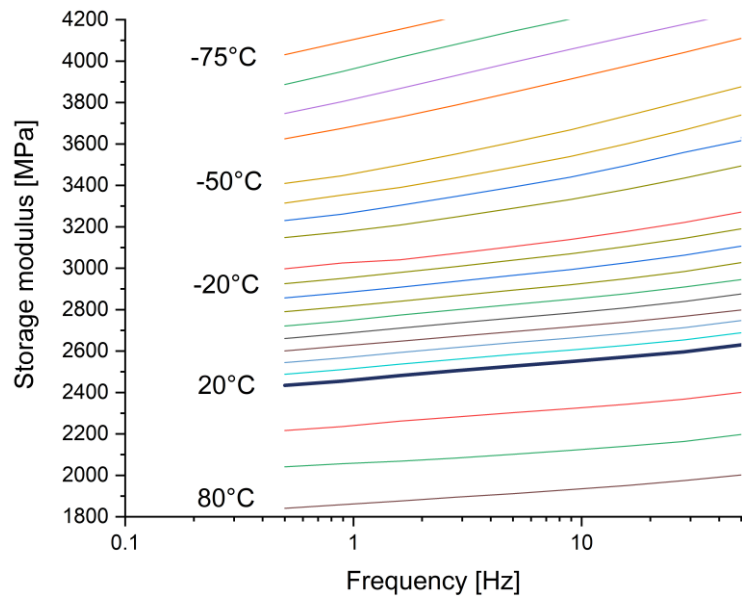
DMA measurement on epoxy resin at 20°C



Measured  
natural  
frequency  
of the  
composite  
drill tube:  
**218 Hz**



# Time-Temperature Superposition



DMA measurement:

- NETZSCH EPLEXOR 2000N
- Temperature-Frequency-Sweep
- 0.5 to 50 Hz; -80 to 90 °C

Approximation by Prony series:

$$E(t) = E_0 \left( 1 - \sum_{i=1}^N g_i (1 - e^{-\frac{t}{\tau_i}}) \right)$$

# Mixing the Matrix and Fiber Properties in an Abaqus User-Material

$$E'_1 = E_{1f} \varphi + E_m (1 - \varphi)$$

$$E''_1 = \frac{E_m}{(1 - \varphi)}$$

Fiber properties:  
non time-dependent

Matrix properties:  
time-dependent

$$E(t) = E_0 \left( 1 - \sum_{i=1}^N g_i \left( 1 - e^{-\frac{t}{\tau_i}} \right) \right)$$

Storage Modulus

$$E'_2 = \frac{E_m}{1 - v_m^2} \frac{1 + 0.85 \varphi^2}{(1 - \varphi)^{1.25} + \frac{E_m}{(1 - v_m^2) E_{2f}} \varphi}$$

$$G'_{12} = G_m \frac{1 + 0.4 \varphi^{0.5}}{(1 - \varphi)^{1.45} + \frac{G_m}{G_{12f}} \varphi}$$

$$v'_{12} = \varphi v_{12f} + (1 - \varphi) v_m \quad v'_{21} = v'_{12} \frac{E'_2}{E'_1}$$

Loss Modulus

$$E''_2 = \frac{E_m}{(1 - \varphi)}$$

$$G''_{12} = \frac{G_m}{(1 - \varphi)}$$

$$v''_{12} = \varphi v_{12f} + (1 - \varphi) v_m \quad v''_{21} = v''_{12} \frac{E''_2}{E''_1}$$

# Modeling of the Drill Tube in Abaqus

| Plies    Offset    Shell Parameters    Display              |          |          |          |           |         |                |                    |
|-------------------------------------------------------------|----------|----------|----------|-----------|---------|----------------|--------------------|
| <input type="checkbox"/> Make calculated sections symmetric |          |          |          |           |         |                |                    |
|                                                             | Ply Name | Region   | Material | Thickness | CSYS    | Rotation Angle | Integration Points |
| 1                                                           | Ply-1    | (Picked) | CF1_UMAT | 0.46      | <Layup> | 6              | 3                  |
| 2                                                           | Ply-2    | (Picked) | CF1_UMAT | 0.46      | <Layup> | -6             | 3                  |
| 3                                                           | Ply-3    | (Picked) | CF1_UMAT | 0.46      | <Layup> | 6              | 3                  |
| 4                                                           | Ply-4    | (Picked) | CF1_UMAT | 0.46      | <Layup> | -6             | 3                  |
| 5                                                           | Ply-5    | (Picked) | GF_UMAT  | 0.46      | <Layup> | 45             | 3                  |
| 6                                                           | Ply-6    | (Picked) | GF_UMAT  | 0.46      | <Layup> | -45            | 3                  |
| 7                                                           | Ply-7    | (Picked) | GF_UMAT  | 0.46      | <Layup> | 45             | 3                  |
| 8                                                           | Ply-8    | (Picked) | GF_UMAT  | 0.46      | <Layup> | -45            | 3                  |
| 9                                                           | Ply-9    | (Picked) | CF1_UMAT | 0.46      | <Layup> | 45             | 3                  |
| 10                                                          | Ply-10   | (Picked) | CF1_UMAT | 0.46      | <Layup> | -45            | 3                  |
| 11                                                          | Ply-11   | (Picked) | CF1_UMAT | 0.46      | <Layup> | 45             | 3                  |
| 12                                                          | Ply-12   | (Picked) | CF1_UMAT | 0.46      | <Layup> | -45            | 3                  |

$t=0.46$  mm

Fixed Displacement/  
Rotation

Composite-Shell

Steel drill head (solid)

Torque:  
Static: 300 Nm  
Dynamic: 0.4 Nm

Evaluation point

Drill head can rotate and shift in Z-direction

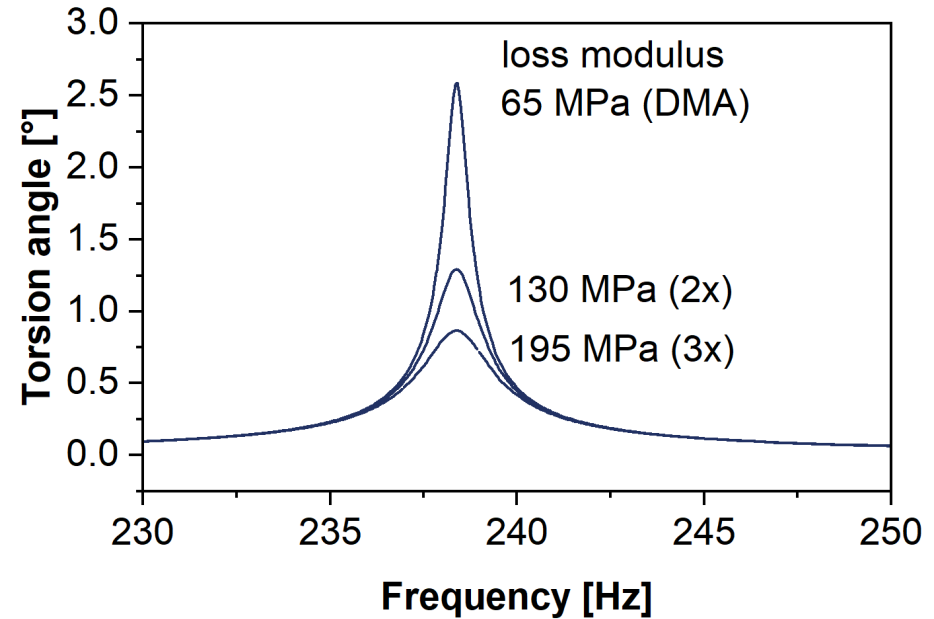
# Results: Influence of the Loss Modulus

## Variation of the loss modulus

- Fiber volume content: 55%

Laminate structure:

$[\pm 6_2^{CF1} / \pm 45_2^{GF} / \pm 45_2^{CF1}]$



Matrix material has great influence on vibration amplitude.

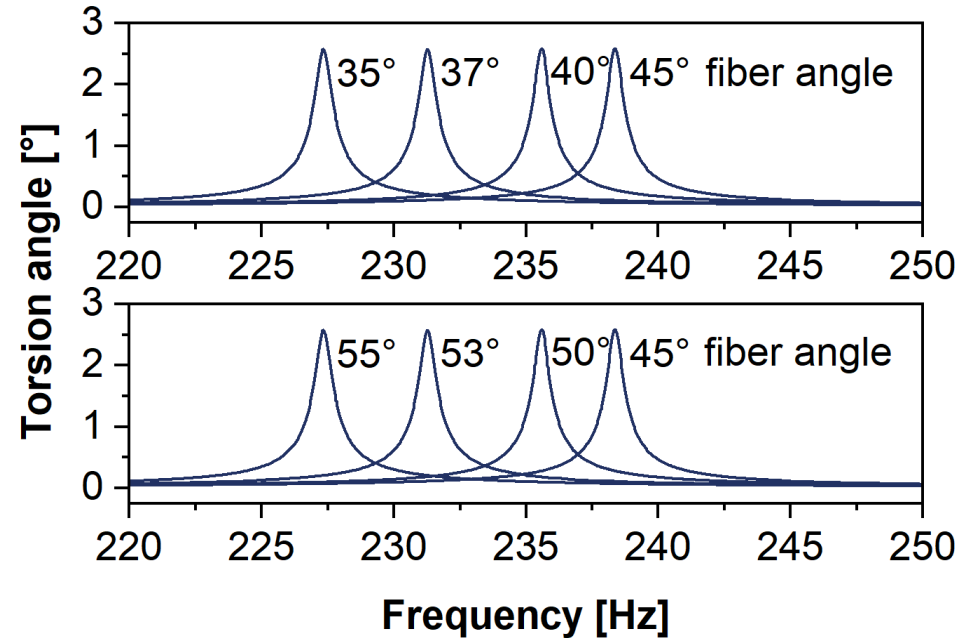
# Results: Influence of the Fiber Angle

## Variation of the fiber angle

- Variation of  $\pm 45^\circ$  layers
- $\pm 6^\circ$  layers for axial load not varied

Laminate structure:

$[\pm 6_2^{CF1}/\pm 45_2^{GF}/\pm 45_2^{CF1}]$



Fiber angle influences natural frequency  
but not vibration amplitude.

# Results: Influence of the Fiber Material

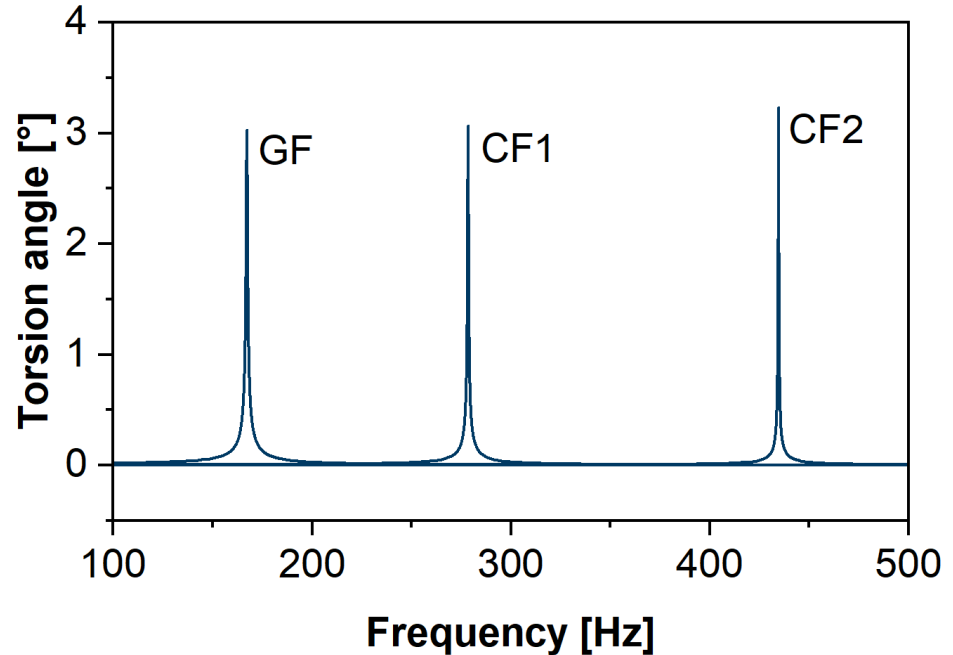
## Variation of the fiber material

- Same fiber material X in all layers
- Fiber volume content: 55%

Laminate structure:

$[\pm 6_2^X / \pm 45_2^X / \pm 45_2^X]$

| Name | Material                                               | Stiffness<br>[GPa] |
|------|--------------------------------------------------------|--------------------|
| CF1  | STS40 F13, 24K, 1600 tex<br>(Toho Tenax)               | 240                |
| CF2  | Dialead K63712, 12K, 2000 tex<br>(Mitsubishi Chemical) | 640                |
| GF   | SE1200, 2400 tex (Owens Corning)                       | 82                 |



Natural frequencies depend significantly on the material. Vibration amplitude is almost the same.

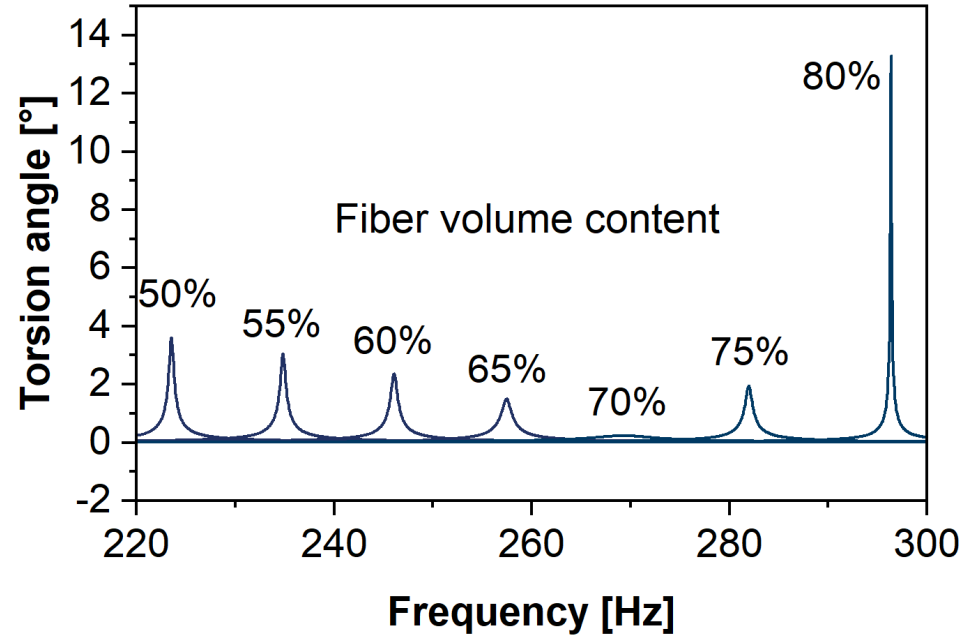


# Results: Influence of the Fiber Volume Content

## Variation of the fiber volume content

Laminate structure:

$[\pm 6_2^{CF1} / \pm 45_2^{GF} / \pm 45_2^{CF1}]$



Increasing the fiber volume fraction from 50 % to 65 % halves the vibration amplitude.

# Conclusion and Outlook

- The use of composite in deep hole drilling tools significantly reduces vibrations
- Model approach for vibration amplitude prediction presented
- Matrix material and fiber volume content influence vibration amplitude
- Fiber material and fiber orientation primarily influence the natural frequency
- Model approach must be validated experimentally
- Comparison of the numerical experiments with real drilling tests is still pending

# Thank you for your attention!

## Project partners:



BGTB GmbH  
Beratende Gesellschaft für  
Tiefbohr- und Zerspanungstechnik



**Fraunhofer**  
IZFP



**carbovation**  
MURTFELDT COMPOSITES



**ISF** INSTITUT FÜR  
SPANENDE FERTIGUNG

**KAISER**  
Maschinenbau

Funded by



Deutsche  
Forschungsgemeinschaft  
German Research Foundation

The authors kindly thank the German Research Foundation (DFG, Project number 426328330) and the Fraunhofer Gesellschaft for the project funding.