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# Fiber orientation tensor approximations based on an implicitly defined closure approach

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- Fiber orientation evolution prediction



Tucker (2022) Figure: Karl et al. (2021)

#### **Motivation**

- Application of short fiber reinforced polymers in lightweight design
- Injection molding process
- Fiber orientation evolution during mold filling
- Final effective anisotropy depends on local fiber orientation



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#### Fiber orientation tensors

Second- and fourth-order orientation tensors of the first kind

$$\mathbf{N} = \int_{\mathcal{S}} f(\mathbf{n}) \mathbf{n} \otimes \mathbf{n} \, \mathrm{d}S$$
$$\mathbb{N} = \int_{\mathcal{S}} f(\mathbf{n}) \mathbf{n} \otimes \mathbf{n} \otimes \mathbf{n} \otimes \mathbf{n} \, \mathrm{d}S$$

Fiber orientation evolution equation

$$\dot{N} = WN - NW + rac{lpha^2 - 1}{lpha^2 + 1} \Big( DN + ND - 2\mathbb{N}[D] \Big) + 2C_{\mathrm{I}}\dot{\gamma}(I - 3N)$$

• Closure function  $\mathbb{F}$  required for closure

 $\mathbb{N} \approx \mathbb{F}(N)$ 

Kanatani (1984) Folgar & Tucker (1984) Advani & Tucker (1987)

### Required algebraic properties of $\mathbb{F}(N)$



- Full index symmetry
- Contraction condition  $\mathbb{N}[I] = N$  or  $N_{ijkk} = N_{ij}$
- Trace condition  $\mathbb{N} \cdot \mathbb{I} = N_{klkl} = 1$
- Trace-preserving property during evolution  $tr(\mathbb{N}[\mathbf{D}]) = \mathbf{N} \cdot \mathbf{D} = N_{ij}D_{ij}$

Advani & Tucker (1987) Petty et al. (1999)

#### Implicit closure approach

Closure tensor B (unknown) is used instead of the given N

 $\mathbb{N} \approx \mathbb{F}(\boldsymbol{B})$ 

 $\mathbb{F}(B)[I] = N$ 

Closure tensor B is implicitly defined via the contraction condition

Function F (whose roots B are sought)

 $F(B) = \mathbb{F}(B)[I] - N$ 

Newton's method

$$\boldsymbol{B}_{n+1} = \boldsymbol{B}_n - \left(\frac{\partial \boldsymbol{F}(\boldsymbol{B}_n)}{\partial \boldsymbol{B}_n}\right)^{-1} [\boldsymbol{F}(\boldsymbol{B}_n)]$$

• If  $\mathbb{F}$  is modeled fully symmetric, all properties of  $\mathbb{N}$  are met



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### Implicit quadratic closure (SIQ)

Chosen closure function

$$egin{aligned} \mathbb{N} &pprox \mathbb{F}(oldsymbol{B}) = ext{sym}(oldsymbol{B} \otimes oldsymbol{B}) \ &= rac{1}{3} \Big( oldsymbol{B} \otimes oldsymbol{B} + oldsymbol{B} oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} + oldsymbol{B} oldsymbol{B} + oldsymb$$

Contraction condition

$$egin{aligned} m{F}(m{B}) &= \mathbb{F}(m{B})[m{I}] - m{N} \ &= rac{1}{3} \Big( ext{tr}(m{B})m{B} + 2m{B}^2 \Big) - m{N} \end{aligned}$$

- Exact for UD, ISO and PI orientation states
- 1D formulation possible

#### Implicit hybrid closure (SIHYB)



Chosen closure function

$$\mathbb{F}(\boldsymbol{B}) = (1-k) \left( -\frac{3}{35} \operatorname{sym}(\boldsymbol{I} \otimes \boldsymbol{I}) + \frac{6}{7} \operatorname{sym}(\boldsymbol{I} \otimes \boldsymbol{B}) \right) + k \operatorname{sym}(\boldsymbol{B} \otimes \boldsymbol{B})$$
$$k = 1 - 27 \operatorname{det}(\boldsymbol{N})$$

Contraction condition

$$\boldsymbol{F}(\boldsymbol{B}) = \frac{1-k}{7} \Big( \operatorname{tr}(\boldsymbol{B}) - 1 \Big) \boldsymbol{I} + \Big( 1 - k + \frac{k}{3} \operatorname{tr}(\boldsymbol{B}) \Big) \boldsymbol{B} + \frac{2k}{3} \boldsymbol{B}^2 - \boldsymbol{N},$$

- Exact for UD, ISO and PI orientation states
- 1D formulation possible



#### **Estimation of effective properties**

Fiber orientation state

$$N_{ij} = \begin{pmatrix} 0.392 & 0.111 & -0.006 \\ 0.111 & 0.584 & -0.005 \\ -0.006 & -0.005 & 0.024 \end{pmatrix}$$

• Mori-Tanaka model with orientation average  $\langle \cdot \rangle_{\mathsf{F}}$ 

$$\begin{split} \bar{\mathbb{C}} &= \mathbb{C}_{M} + c_{F} \Big( c_{F} \delta \mathbb{C}^{-1} + c_{M} \big\langle \big( \delta \mathbb{C}^{-1} + \mathbb{P}_{0} \big)^{-1} \big\rangle_{F}^{-1} \Big)^{-1} \\ \bar{\mathbb{V}} &= \mathbb{C}_{M} + \frac{c_{F}}{c_{M}} \big\langle \mathbb{P}_{0}^{-1} \big\rangle_{F} \end{split}$$

Aspect ratio \alpha = 26

- Fiber volume fraction c<sub>F</sub> = 0.13
- PP matrix (E = 1.6 GPa,  $\nu = 0.4$ ) and glass fibers (E = 73 GPa,  $\nu = 0.22$ )

Müller et al. (2016) Mori & Tanaka (1973) Benveniste (1987) Schürmann (2007) Bertóti & Böhlke (2017)



#### **Effective stiffness**





#### **Effective viscosity**









#### Fiber orientation evolution (shear flow, $\alpha ightarrow \infty$ )



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### Summary and conclusion

- Implicit closure approach based on contraction condition
- Fully symmetric implicit closure meets all algebraic requirements
- ID formulation for both quadratic and hybrid approach
- Reliable estimation of anisotropic properties
- Fiber orientation evolution shows oscillations in simple shear flow
- Low-cost MEM approximation

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#### Appendix: Computational effort

Absolute computation time $t_c$ and approxi-		
mate relative	computation tim	le $t_{rel}$ for all
considered closure approximations.		
Closure	$t_{\rm c}$ in s	$t_{\rm rel}$ in %
MEM	0.31688170	486024
ACG	0.11489970	176230
SIHYB	0.00011718	180
SIQ	0.00007490	115
IBOF	0.00006520	100
HYB	0.00001681	26
SQC	0.00000697	11
QC	0.00000186	3

#### Appendix: 1D formulation of SIQ



• F(B) = 0 can be written as follows with s = tr(B)/4

$$B^2+2sB=rac{3}{2}N$$

Completing the square

$$(\boldsymbol{B}+\boldsymbol{s}\boldsymbol{l})^2=\frac{3}{2}\boldsymbol{N}+\boldsymbol{s}^2\boldsymbol{l}$$
  $\iff$   $\boldsymbol{B}=\sqrt{\frac{3}{2}\boldsymbol{N}+\boldsymbol{s}^2\boldsymbol{l}}-\boldsymbol{s}\boldsymbol{l}$ 

Trace of both sides (*B* and *N* share the same eigensystem)

$$(d+4)s = \sum_{i=1}^d \sqrt{\frac{3\lambda_i}{2} + s^2}$$

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#### Appendix: 1D formulation of SIQ

• Newton's method for s (fixed  $\lambda_i$  and d)

$$f(s)=(d+4)s-\sum_{i=1}^d\sqrt{rac{3\lambda_i}{2}+s^2}$$
 $f'(s)=4+\sum_{i=1}^d\underbrace{\left(1-rac{s}{\sqrt{rac{3\lambda_i}{2}+s^2}}
ight)}_{\geq 0}\geq 4$ 

Eigenvalues of **B** 

$$\mu_i = \sqrt{\frac{3\lambda_i}{2} + s^2} - s$$

### **Appendix: References**



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