Investigations on interactive failure mechanism of a laminated composite using synchrotron radiation computed tomography and finite element analysis

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Motivation and Purpose

Motivation

- -Complex failure mechanism of laminated composite
 - Anisotropy, heterogeneity, multi-scale, interactive failure modes
 - Internal damage progression
- -Understanding of failure mechanism
 - Optimal design of laminated composite
 - Validation of numerical model

Trends and Limitations

- -Time-lapse high-resolution X-ray CT imaging
 - 3D visualization and history of multiscale cracks
 - Limited to the pre-peak zone

Objectives







Ni et al. Compos. B. Eng, (2021)

Scott et al. Compos Sci Technol, (2011)

- -Experimental investigations of interactive failure mechanisms in a cross-ply laminated composite while the materials form maximum load point
- -Finite element analysis for supplementing the experimental observation

Materials and Specimens

- [Carbon fiber / Epoxy] laminated composite
 - -Autoclave process using UD carbon fiber-reinforced epoxy prepreg
 - UIN150/H15 prepreg (SK chemicals, South Korea)
 - Fiber volume fraction ~ 57%
- $[+45_2/-45_2]_s$ off-axis tensile specimen
 - -Cut using a water jet
 - -Focus on the interaction of matrix crack and delamination
 - -Standard test specimen for in-plane shear response (ASTM D3518)
 - -Dimensions based on a miniature tensile loading machine and inspection system



Tensile Behavior

- Response of the $[+45_2/-45_2]_s$ sample under tensile loading
 - -Miniature loading stage (MT 2000, Deben Ltd, UK)
 - Maximum capacity of 2 kN
 - Displacement-controlled loading rate : 0.1 mm/min
 - Force data : Load cell
 - Displacement data : Linear extensometer
 - -Residual load-carrying capabilities after the significant load drop
 - -Peak stress: 92.74 (± 1.53) MPa
 - -Strain at peak: 1.339 (± 0.091)





Preparation of Specimen for CT Imaging

- Interrupted specimens for the non-destructive X-ray inspection
 - -Tensile tests were manually interrupted near the peak stress
 - As soon as the real-time force measurement began to decrease
 - -Unstable specimens were stopped either near the peak stress (NP) or after-peak stress (AP)
 - -Ex-situ observation using SRCT
 - Dye penetrant

| Specimen | Peak stress (and strain) | Interruption stress (and strain) | Dyeing |
|----------|-----------------------------|-------------------------------------|--------|
| NP1 | 92.04 (1.317) | 91.84 (1.322) | Dyed |
| NP2 | 92.71 (1.328) | 92.60 (1.339) | Dyed |
| AP1 | 91.93 (1.228) | 6.927 (1.872) | Undyed |
| AP2 | 96.16 (1.378) | 17.59 (1.539) | Dyed |



SRCT Setup for Crack Visualization

- Two different settings according to dye usage
 - -Dyed setting for observation the cracks hidden inside the samples
 - Znl₂-based dye solution penetrates and deposits on crack surfaces
 - -Undyed setting for distinguish the carbon fibers from the epoxy matrix
 - -Key parameters : Beam voltage, Sample-to-detector distance (SDD)

| | Dyed | Undyed | | |
|----------------------|-------------------------------------|---------------------------|--|--|
| Beam voltage | 35.5 keV | 25 keV | | |
| Beam current | 250 mA | | | |
| Monochromator | DMM | DCM | | |
| Exposure time | 50 ms | 500 ms | | |
| SDD | 100 mm | 45 mm | | |
| FOV size | $3.3 \times 2.8 \text{ mm}^2$ | 4.16×3.51 mm ² | | |
| (Pixel size) | (1.3 µm) | (1.625 µm) | | |
| Scintillator | 100 μ m thick CdWO ₄ | | | |

Reconstruction

- -3,000 projection images during 180° rotation
 - Reconstruct 2,160 tomograms using Octopus (XRE, Gent, Belgium)



6C beamline at Pohang Accelerator Laboratory (PAL)

Damage Pattern with SRCT

- Unique failure pattern
 - -A single fully-developed matrix crack in either outside +45° or inside -45° layers \rightarrow "Primary crack"
 - -Multiple immature cracks in the other orientation layers
 - -NP1, AP1 : Primary crack was found in the inside -45° layer



Front view



- \checkmark Initiation of the delamination failure
 - From the edges of the primary crack in the -45° layers
 - Release of accumulating strain energy by turning the crack paths through the interfaces
 - Bifurcation occurred near the interfaces
 - Delamination was transitioned from the matrix crack
- ✓ Minor matrix cracks in +45° layers
 - Branch off from the primary crack band

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Damage Pattern with SRCT

Unique failure pattern

-NP1, **AP1** : Primary crack was found in the inside -45° layer



Front view

Summary of Damage Pattern in NP1 and AP1

Unique failure pattern





- ✓ Sequential and interacting failure process between the matrix crack and delamination
 - Initiation of delamination from the internal primary crack
 - Load transfer to the outside $+45^{\circ}$ layers \rightarrow Initiation of multiple matrix cracks
 - Growth of the +45° cracks in the transverse direction \rightarrow Additional delamination
 - One of the transverse cracks in each of the +45° layers further grew into a "primary crack" \rightarrow Separation into two parts

Damage Pattern with SRCT

- Unique failure pattern
 - -NP2, AP2 : Primary crack was found in the inside +45° layer



Front view

45°

View A

- ✓ Similar but opposite failure process
 - Only one primary crack in each of the +45° layers
 - Multiple immature cracks in the -45° layers
- $\checkmark\,$ Interactive failure process
 - (1) Primary cracks in the +45° layers
 - 2 Initiation of delamination
 - \bigcirc Load transfer to the -45° layers
 - (4) Multiple cracks in the -45° layers
 - Growing of the multiple cracks in the thickness direction and fiber direction
 - 6 Additional delamination

Damage Pattern with SRCT

Unique failure pattern

-NP2, **AP2** : Primary matrix crack was found in the inside +45° layer



- Can be considered the next stage of the NP2 specimen
 - Growing of the multiple cracks in the -45° layers
 - Expansion of interfacial failure
- ✓ No separation after load-drop
 - No primary cracks in the -45° layers
 - Not sufficiently developed delamination

Summary of Damage Pattern in NP2 and AP2

• Unique failure pattern





- ✓ Sequential and interacting failure process between the matrix crack and delamination
 - Initiation of delamination from the external primary crack
 - Load transfer to the inside -45° layers \rightarrow Initiation of multiple matrix cracks
 - Growth of the -45° cracks in the transverse direction \rightarrow Additional delamination
 - One of the transverse cracks in the -45° layer further grew into a "primary crack" \rightarrow Separation into two parts

Finite Element Analysis

- Heterogeneous model configuration
 - -Consider fiber-level fracture behavior with computational efficiency
 - Diameter of scaled-up fibers : 0.22 mm
 - Thickness of interface : 0.03 mm
 - Fiber volume fraction : 57.1 %
 - 337,746 Quadratic tetrahedral elements
 - -Fiber shift : Artificial stress concentration between a fiber pair
 - Fiber shift in the -45° layer : "Model M"
 - Fiber shift in the +45° layer : "Model P"





Material Model and Input Parameters

Material models

-Fiber : Transversely isotropic & Linear elastic

| *E ₁₁ | $**E_{22} = E_{33}$ | $***G_{12} = G_{13}$ | **G ₂₃ | $**\nu_{12} = \nu_{13}$ | ** v ₂₃ | * ρ |
|------------------|---------------------|----------------------|-------------------|-------------------------|---------------------------|-----------------------|
| 290 GPa | 19 GPa | 18.1 GPa | 7 GPa | 0.2 | 0.2 | 1.81 g/cm^3 |

- -In situ matrix : Isotropic & Elasto-plastic & Post-peak strain softening
 - Johnson-Cook plasticity and damage model (available in ABAQUS)
 - Assumption: Damage initiation is independent of triaxiality, strain rate, and temperature

| Ε | ν | σ_Y | $\overline{\epsilon}_{D}^{pl}$ | G _c | ρ |
|-----------|------|------------|--------------------------------|----------------|----------------------|
| 3.354 GPa | 0.33 | 39.97 MPa | 0.03 | 0.169 N/mm | 1.2 g/cm^3 |

- Modulus (E), Nonlinear behavior : Inverse-analysis approach^[1]
- Yield strength (σ_Y) : Where the secant stiffness is equal to 99% of the initial stiffness
- Critical equivalent plastic strain $(\overline{\epsilon}_{D}^{pl})$: Virtual V-notched shear test
- Damage evolution energy (G_c) : Mode I fracture energy^[2]

* Toray, T800H Technical Data sheet, (2018)

^{**} Kaddour et al, J. Compos. Mater., (2013)

^{***} Kumar, Znt. SAMPE Symp. and Exhib., (1990)

FEA result – Global Responses

Global responses

- -Successfully reproduction in the pre-peak region
 - Validation of modeling scheme to represent the effective properties of the laminated composite
- -Earlier break than the experimental measurements
 - Simplification of the real microstructure \rightarrow Nonuniform stress distribution
- Damage analysis
- Initiation of "primary crack" between the shifted fiber-pair
- Matrix failure index: Scalar stiffness degradation variable (SDEG)
 - "0" before the equivalent plastic strain of an element reaches $\overline{\epsilon}_D^{pl}$
 - "1" when fracture energy is entirely released



FEA result – Damage Pattern

• Model M (Fiber shift in -45° layer)





Note) Visualizing the elements with SDEG being greater than 0.8

FEA result – Damage Pattern

Model P (Fiber shift in +45° layer) +45° layer (Bottom) Matrix crack in bottom +45° a (\mathbf{b}) . K **~*** Matrix crack in top +45° +45° layer (Top) Matrix cracks in top and bottom +45° Matrix cracks in middle -45° Interface cracks extended from the \bigcirc transverse cracks in +45° Multiple transverse matrix cracks in -45° ×v 1 Interface cracks



Note) Visualizing the elements with SDEG being greater than 0.8

Conclusion



- Interactive failure process during the rapid loss of load-bearing capacity
 - (1) A single fully-developed matrix crack (primary crack) in either +45° or -45° layers
 - ② Delamination initiated from the primary cracks
 - ③ Multiple immature cracks in the other orientation layers
 - ④ Growth of delamination due to the multiple cracks
 - (5) One of the multiple cracks grows into fully-developed matrix crack
 - 6 Separation into two parts

Shear strength determining mechanism

Thank you for your attention

Appendix

Input parameters for the matrix material



Appendix

