Interfacial Toughening of Hybrid Metal-Composite Joints Using 3D Printed Pins

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In collaboration with DSTG with approved DSI scholarship







Introduction



Quasi-Static Results



Mode I Fatigue







Introduction



Quasi-Static Results



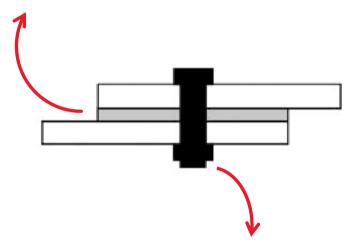
Mode I Fatigue



RMIT Classification: Public

Adhesive

- Specific surface preparation
- Can fail catastrophically



Mechanical Fasteners

- Adds weight
- Damages composite

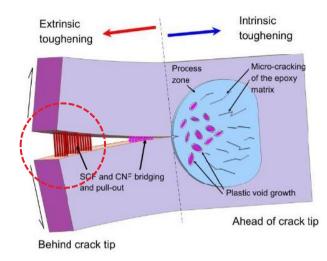


Figure 01. Toughening mechanisms of reinforcements, Ravindran A.

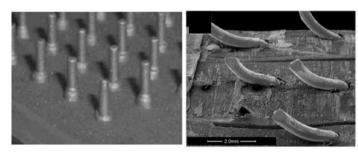


Figure 02. Left; Steel CMT pins (Ucsnik S.), Right; Steel z-pins (Ravindran A.)





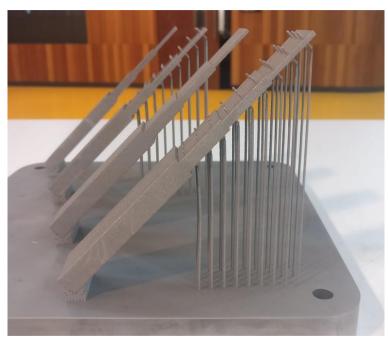


Figure 03. 3D printed titanium multi-step lap joints

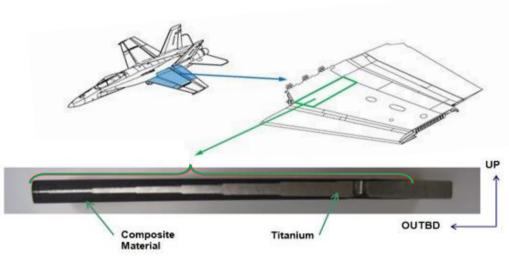


Figure 04. F/A18A-D hybrid titanium-CFRP multi-step lap joint, Mouritz A. et al.





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As-Manufactured Pin Features



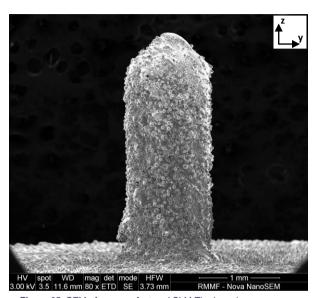


Figure 05. SEM of as-manufactured SLM Ti-micro pin

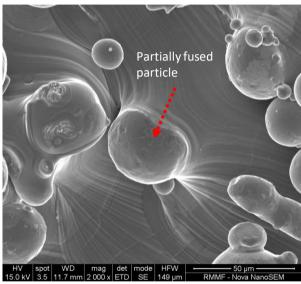


Figure 06. High magnification SEM image of partially fused titanium particles

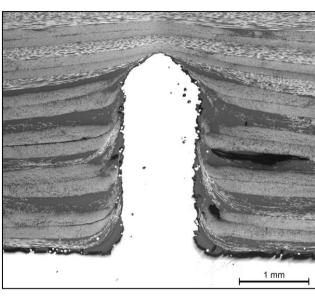


Figure 07. Cross-section of in-situ micro pin

- As-manufactured pin surface roughness: $7 \pm 0.75 \mu m$
- CFRP experiences fibre crimping and eyelet formation

Mode I – Quasi-Static Testing



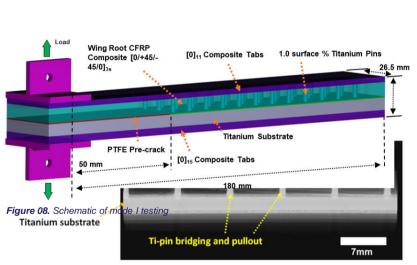
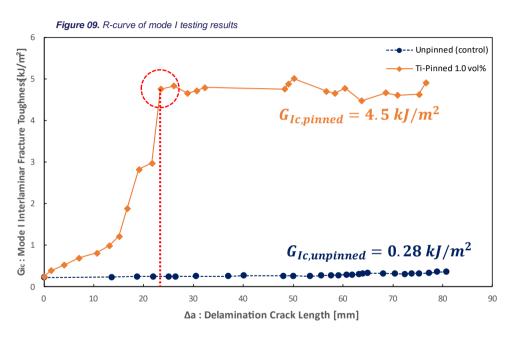


Figure 10. X-ray CT image of micro-pin bridging zone under mode I loading



Improvement of ~1600% from unpinned to pinned specimen

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Single Pin Pull-Out Testing



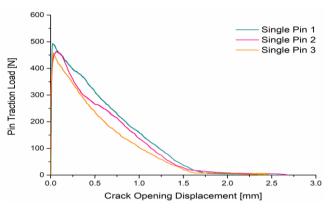


Figure 11. Pin traction load vs crack opening displacement results

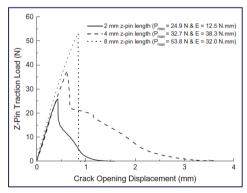
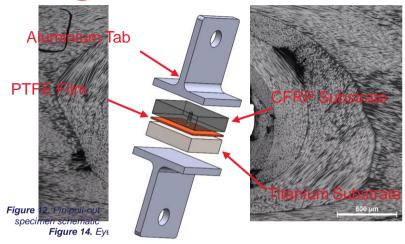


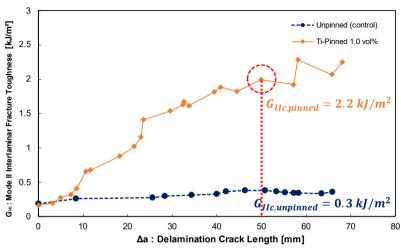
Figure 13. Typical Z-Pin traction load vs displacement graph, Mouritz et al.

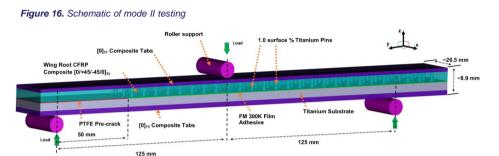


- Average peak load and pull-out traction energy;
 472N and 337 N.mm respectively
- CTE values, pull-out results and optical microscopy imaging suggest the pin is entirely debonding from the surrounding matrix

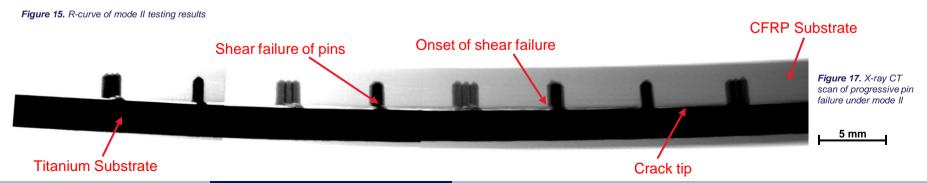
Mode II - Quasi-Static Testing







Improvement of ~500% from unpinned to pinned specimen



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Introduction



Quasi-Static Results

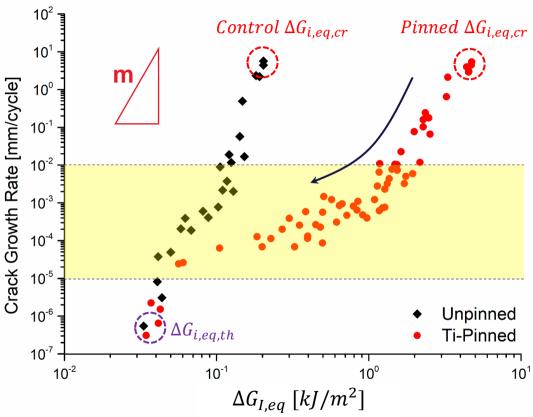


Mode I Fatigue



Interlaminar Fatigue – Mode I





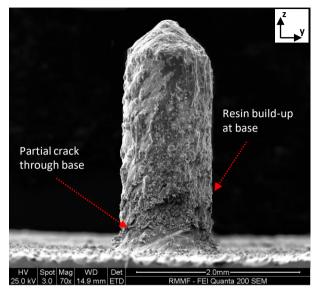
R-ratio of 0.1 at 5 Hz

- Load shedding scheme
- $m_{unpinned} = 5.343$
- $m_{Ti-pinned} = 0.833$

Figure 17. Paris-like curve of mode I interlaminar fatigue results

Interlaminar Fatigue – Mode I





Fractured imbedded Ti-pin **CFRP** substrate

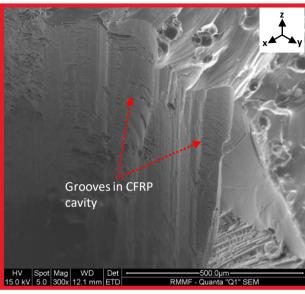


Figure 18. SEM image of Ti-pin after mode I fatigue testing

Figure 19. SEM image of fractured Ti-pin embedded in CFRP laminate

Figure 20. High magnification SEM image of CFRP cavities

- Pin undergoes large tensile and compressive loads
- Gradual pin fracture further resists interlaminar cracking
 - Widening of CFRP grooves worsens through-out test

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Interlaminar Fatigue – Single Pin Pull-Out



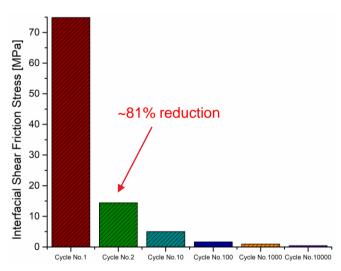


Figure 21. Interfacial shear friction stress bar chart

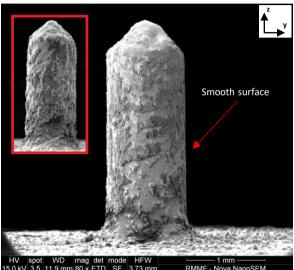


Figure 22. SEM image of single pin pull-out fatigue Ti-pin after 30 000 cycles (boxed: Mode I fatigue pin)

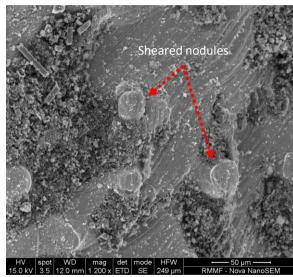
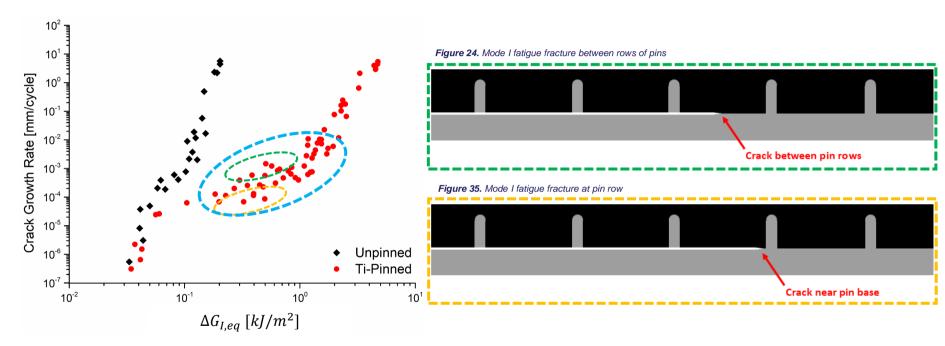


Figure 23. High magnification SEM image of sheared titanium nodules

Interlaminar Fatigue – Mode I





- Larger crack growth rate at given strain energy release rate for crack location between pins
- Smaller crack growth rate at given strain energy release rate for crack location at pin row

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Quasi-Static Results

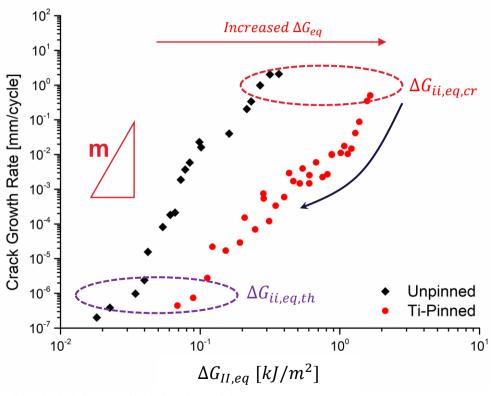


Mode I Fatigue



Interlaminar Fatigue – Mode II





- R-ratio of 0.1 at 5 Hz
- Load shedding scheme
- $\uparrow \Delta G_{II,eq,th} \approx 167\%$
- $m_{unpinned} = 2.622$
- $m_{Ti-pinned} = 2.008$

Figure 26. Paris-like curve of mode II interlaminar fatigue results

Interlaminar Fatigue – Mode II







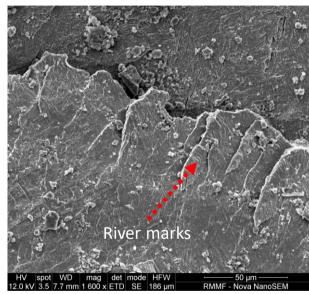


Figure 27. Ti-pin embedded in CFRP laminate; high SERR region

Figure 28. Ti-pin embedded in CFRP laminate; low SERR region

Figure 29. High magnification SEM image of river marks

- Plasticisation of pins under shear → absorbing energy from crack front
 - River marks evident showing crack progression and direction

Interlaminar Fatigue – Mode II



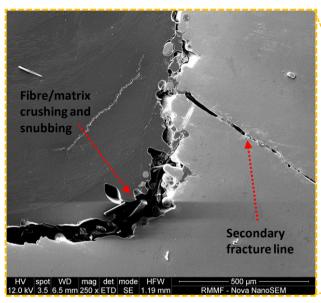


Figure 30. High magnification SEM image of secondary fracture line and snubbing

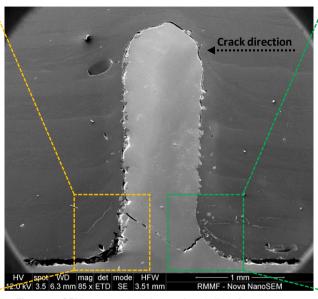


Figure 31. SEM cross sectional image of mode II pin fracture

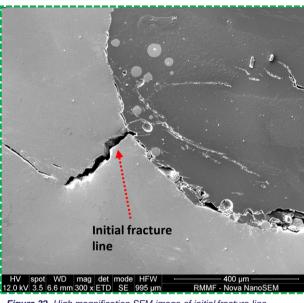


Figure 32. High magnification SEM image of initial fracture line

- Pin fracture captured in two stages
- Fracture propagates along print plane upon pin weakening
 - Snubbing absorbs energy from crack front

Summary



- Improvement of interlaminar fracture in the pinned joints is higher under mode
 I due to bridging zone formation
- Mode I fatigue fraction resistance is mainly due to the lateral pressing of pins on CFRP wall
- Mode II fatigue fracture resistance is mainly due to 2-stage pin fracture as well as fibre/matrix crushing and snubbing

Further information on research:

- Bagnato et al., "Superior interfacial toughening of hybrid metalcomposite structural joints using 3D printed pins", Composites Part A
- "Interfacial fatigue performance of hybrid titanium-composite joints reinforced with 3d printed pins" – Undergoing review







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Dr. John Wang

Dr. Paul Chang

DSTG and DSI Scholarship representatives
Composites lab team
Materials and structures lab team

Thank you for listening

Questions are welcome!

